

the geometries considered in [1]–[5], eq. (1) has a scalar form and, according to the theory of the modal representations of electromagnetic fields in closed waveguides,  $G(\alpha)$  must be a meromorphic function having zeros at the modal propagation constants  $\pm j\gamma'_n$  of the guide  $a'$  and poles at the modal propagation constants  $\pm j\gamma_n$  of the guide  $a$ . With these conditions, a Weierstrass factorization of  $G(\alpha)$  leads straightforwardly to expressions of scattering coefficients having the forms given in [1, eqs. (50) and (51)]. A different situation occurs when (1) has a matrix form. In this case, a considerable effort has been made in the past by one of the authors to obtain a closed-form solution [3]. Even if some progress has been accomplished, a general solution of a matrix Wiener–Hopf equation is not available. From the previous considerations it follows that 1) a general criterion on the validity of the scattering coefficients given in [1] has to be based on the scalarization of the Wiener–Hopf formulation of the problem at hand, and 2) more general approximate solutions have to be worked out by using, on the W–H formulation, the powerful methods developed in the literature (see, for example, [6]). Those solutions, with respect to the perturbational one proposed in [1], have a deeper mathematical justification.

Reply<sup>2</sup> by C. Dragone<sup>3</sup>

A junction between two waveguides can, under certain general conditions derived in [1], be represented by a scalar Wiener–Hopf equation. Then, as shown in [2], the junction can be treated rigorously by either one of two well-known methods.

The authors of the above comments criticize the mode-matching technique used in [1] and claim that a rigorous treatment of a junction can only be given by the Wiener–Hopf technique, as shown by their work in [5]. They also claim that all geometries considered in [1] are described by a scalar Wiener–Hopf equation. Furthermore, they question the utility of the perturbation solution of [1].

The above two techniques are well known, and their validity is well established [7]. They are based on two different representations of a junction. One representation involves the Fourier transform of the field along the axis, and leads in general to two integral equations. The other, leads to an infinite set of equations, as in [1]. The two representations are entirely equivalent. Under certain conditions, one representation can be reduced to a scalar integral equation of the Wiener–Hopf type. Under the same conditions, the infinite set of equations will assume a simple form, which can also be solved straightforwardly as shown in [1]. The two representations are well known [7], they are equally important, and either one can be obtained from the other by suitable transformations. In [1], the former representation was used in order to derive some of the results and, in particular, to obtain the perturbation solution. Perturbation solutions are important, particularly when better solutions are not available. They are widely used in the treatment of small imperfections or discontinuities in waveguides and in numerous other applications. Of course, since the perturbation solution in [1] is derived from an infinite series, it only applies if the series converges [8].

The results of [1] imply that the problem can be reduced, under certain conditions, to a scalar Wiener–Hopf equation. This is obvious, in view of the form of the solution given in Section V, and it can also be verified without difficulty using the method of [6]. However, the geometries of [1] are not in general described by a scalar Wiener–Hopf equation. In fact, the perturbation analysis of Section IV shows that the solution given in Section V is only

possible under certain conditions: If the coefficients  $M_{n,l}$  are separable and, furthermore, either  $(X - X')(Y - Y') = 0$  or  $X - X' = Y - Y'$ . The former condition is not satisfied by the horn of [9]. Then, a solution in the form of [1, eq. (50)] is not possible.

## REFERENCES

- [1] C. Dragone, "Scattering at a junction of two waveguides with different surface impedances," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-32, pp. 1319–1328, Oct. 1984.
- [2] V. Daniele and R. Zich, "Coupling of two semi-infinite circular waveguides with anisotropic surface admittance," *Atti Accademia delle Scienze di Torino*, vol. 109, pp. 481–491, 1975.
- [3] V. Daniele, "Coefficienti di accoppiamento nella giunzione tra due guide d'onda delimitate da superfici di impedenza," in *II Riunione Nazionale di Elettromagnetismo Applicato*, (Pavia), Oct. 2–4, 1978, pp. 165–172.
- [4] V. Daniele, I. Montrosset, and R. Zich, "Calcolo della matrice di diffusione nella giunzione tra due guide corrugate," in *IV Riunione Nazionale di Elettromagnetismo Applicato*, (Firenze), Oct. 1982, pp. 313–315.
- [5] V. Daniele, I. Montrosset, and R. Zich, "Wiener–Hopf solution for the junction between a smooth and a corrugated cylindrical waveguide," *Radio Sci.*, vol. 14, pp. 943–956, 1979.
- [6] B. Noble, *Methods Based on the Wiener–Hopf Technique for the Solution of Partial Differential Equations*. London: Pergamon Press, 1958, pp. 153–160.
- [7] R. Mittra and S. W. Lee, *Analytical Technique in the Theory of Guided Waves*. New York: MacMillan, 1971.
- [8] S. A. Schelkunoff, "Conversion of Maxwell's equations into generalized telegraphist's equations," *Bell Syst. Tech. J.*, pp. 994–1043, 1955.
- [9] C. Dragone, "A rectangular horn of four corrugated plates," *IEEE Trans. Antennas Propagat.*, vol. AP-33, pp. 160–164, Feb. 1985.

## Correction to "A Novel Quasi-Optical Frequency Multiplier Design for Millimeter and Submillimeter Wavelengths"

JOHN W. ARCHER, SENIOR MEMBER, IEEE

In the above paper,<sup>1</sup> there is a typographical error in an equation on p. 424, first column. This should read:

"... Above cutoff the power transmission ( $T$ ) is given, for normal incidence, by [16]

$$T^2 = 4 / \left( 4 \left( C - \frac{B_s}{Y_2} S \right)^2 + \left( \frac{Y_1}{Y_2} S + 2 \frac{B_s}{Y_1} C + \frac{Y_2}{Y_1} S - \frac{B_s^2}{Y_1 Y_2} S \right)^2 \right)$$

where..."

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<sup>1</sup>J. W. Archer, *IEEE Trans. Microwave Theory Tech.*, vol. MTT-32, pp. 421–427, Apr. 1984.

## Correction to "Design of Nonradiative Dielectric Waveguide Filters"

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In the above paper,<sup>1</sup> Figs. 1 and 7 should be interchanged.

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<sup>1</sup>T. Yoneyama, F. Kuroki, and S. Nishida, *IEEE Trans. Microwave Theory Tech.*, vol. MTT-32, pp. 1659–1662, Dec. 1984.

<sup>2</sup>Manuscript received March 29, 1985.

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